



# Biodiesel production direct from high acid value oil with a novel magnetic carbonaceous acid



Fan Zhang<sup>a,b</sup>, Zhen Fang<sup>a,\*</sup>, Yi-Tong Wang<sup>a,b</sup>

<sup>a</sup> Chinese Academy of Sciences, Biomass Group, Key Laboratory of Tropical Plant Resources and Sustainable Use, Xishuangbanna Tropical Botanical Garden, 88 Xuefulu, Kunming, Yunnan Province 650223, China

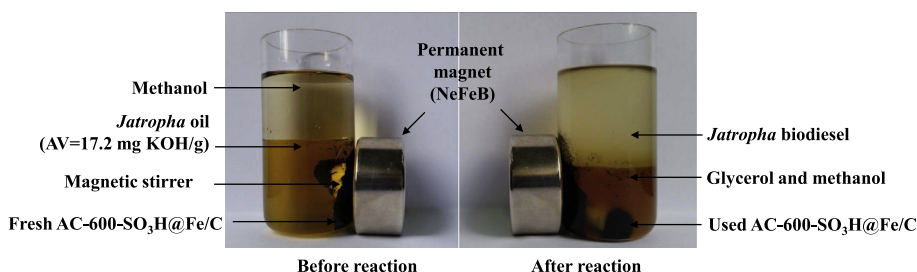
<sup>b</sup> University of Chinese Academy of Sciences, 19A Yuquan Road, Beijing 100049, China

## HIGHLIGHTS

- A novel route with five steps to produce a new magnetic carbonaceous acid.
- The catalyst has high acid content (2.79 mmol/g) and magnetism (14.4 Am<sup>2</sup>/kg).
- 91.8% *Jatropha* biodiesel yield is achieved with the catalyst directly.
- The catalyst is stable for 3 cycles with biodiesel yield >90% at AV of 17.2.
- The recovery rate of catalyst is 96.3% after 3 cycles.

## GRAPHICAL ABSTRACT

A novel magnetic carbonaceous acid catalyst was synthesized from glucose and iron chloride by a new method of double hydrothermal precipitation and pyrolysis, and subsequent sulfonation. The catalyst presents high active, stable and recoverable in the production of *Jatropha* biodiesel with high yields for 3 cycles (90.5%, 91.8%, 90.3%), slight reduction in total acid density (2.43 vs. 2.79 mmol/g) and high catalyst recovery rate of 96.3%.



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## ABSTRACT

A novel magnetic carbonaceous acid catalyst was synthesized from glucose and iron chloride by a new method of double hydrothermal precipitation at 180 °C and pyrolysis at 400–800 °C, and subsequent sulfonation at 150 °C. Its crystalline phases, magnetic saturation (Ms), morphology, specific surface area, pore volume, functional groups, thermal stability, elemental composition and total acid density were analyzed with various techniques. It was found that catalyst carbonized at 600 °C (AC-600-SO<sub>3</sub>H@Fe/C) had high acid density (2.79 mmol/g) and strong magnetism (Ms: 14.4 Am<sup>2</sup>/kg) for direct production of biodiesel from *Jatropha* oil with high acid value (17.2 mg KOH/g) by single-factor optimization. With the catalyst, 90.5% biodiesel yield was achieved at 200 °C with 3 cycles (>90% yield) and 96.3% catalyst recovery rate. The magnetic catalyst directly esterified and transesterified high acid value oil without pretreatment with high biodiesel yield and easily separated for three recycles with little deactivation. It could also find other applications such as pretreatment of oils with high AV and hydrolysis of biomass.

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## 1. Introduction

Due to limited fossil resources and greenhouse gas emissions caused by the combustion of fossil fuels, the researches for converting renewable biomass to alternative fuels have gained much attention [1,2]. Biodiesel [3] is considered as a good alternative

\* Corresponding author. Tel.: +86 871 65137468; fax: +86 871 65160916.

E-mail address: [zhenfang@xtbg.ac.cn](mailto:zhenfang@xtbg.ac.cn) (Z. Fang).

URL: <http://brg.groups.xtbg.ac.cn/> (Z. Fang).

for fossil fuels because it is clean, renewable and carbon neutral [4]. Biodiesel production by transesterification catalyzed by base heterogeneous catalysts, such as modified CaO [5], KF/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>/honeycomb [6] and sodium silicate [7] are widely studied because they are easier recovered than homogeneous ones [8]. However, the technology based on these base catalysts requires using crude oils with low free fatty acids (FFAs) to avoid saponification [9]. So, solid acid catalysts, such as macroporous cation exchange resin [10], heteropoly acid [11] and sulfonated metallic oxides (e.g., zirconia, tin and titanium oxide) [12–14] are studied to produce biodiesel from high FFA oils.

Sulfonated activated carbon (AC-SO<sub>3</sub>H) can also catalyze both esterification and transesterification to produce biodiesel from oils with high acid value (AV) without pretreatment [15,16]. Because, AC has properties like its surface oxides [17], reducibility [18], and stability in both acidic and basic media [19], as well as its structural resemblance to graphite [20], fullerenes [21] and nanotubes [22] to support –SO<sub>3</sub>H well. However, the separation of AC-SO<sub>3</sub>H catalyst needs filtration or centrifugation [23] that is energy and time consuming. So, many magnetic carbonaceous acids were successfully prepared that are easily separated by a magnet, such as Fe<sub>3</sub>O<sub>4</sub>@C-SO<sub>3</sub>H [24], magnetic lignin-derived amorphous carbon solid acid (MLC-SO<sub>3</sub>H) [25] and sulfonated magnetic carbon nanotube arrays (sulfonated MCNAs) [26] for cellulose hydrolysis, fructose dehydration and hydrolysis of polysaccharides in crop stalks (Table 1). But these catalysts have low acid content (1.3, 1.95 and 0.38 mmol/g) for effective biodiesel production, some have low magnetism [e.g., for sulfonated MCNAs with only magnetic saturation (Ms) of 6.32 Am<sup>2</sup>/kg before sulfonation].

This work aims to synthesize magnetic carbonaceous acids with high acidity and strong magnetism for biodiesel production from oils with high acid value. First, magnetic core is formed by hydrothermal precipitation from both glucose and iron chloride and subsequent high temperature pyrolysis. The core is again hydrothermally coated with glucose and stabilized by pyrolysis, and subsequent sulfonated as acid catalyst for *Jatropha* biodiesel production.

## 2. Experimental

### 2.1. Materials

Analytical reagents FeCl<sub>3</sub>·6H<sub>2</sub>O (≥99.0%), glucose (≥99.0%), urea (≥99.0%), H<sub>2</sub>SO<sub>4</sub> (≥98.0%) and dehydrated methanol

(≥99.5%) were purchased from Xilong Chemical Factory Co., Ltd., (Shantou, Guangdong). Standard heptadecanoic acid methyl ester (HDAM; C<sub>17:0</sub>) and other methyl esters [palmitate (C<sub>16:0</sub>), linolenate (C<sub>16:1</sub>), stearate (C<sub>18:0</sub>), oleate (C<sub>18:1</sub>), linoleate (C<sub>18:2</sub>) and linolenate (C<sub>18:3</sub>)] (≥99.0%) were purchased from Sigma (Shanghai). Crude *Jatropha* oil (stored for five years) was obtained from our Garden in Xishuangbanna (Yunnan). According to the Chinese National standards (GBT 5530-2005 and 5534-2008), AV and saponification value (SV) of the crude *Jatropha* oil were measured by titration as 17.2 mg KOH/g and 195.7 mg KOH/g, respectively. So the molecular weight is 942.9 g/mol calculated by the formula  $[M = (56.1 \times 1000 \times 3)/(SV - AV)]$  [27].

### 2.2. Preparation of catalyst

A novel route with five steps by double hydrothermal precipitation and pyrolysis, as well as sulfonation was used for the catalyst synthesis:

(i and ii) magnetic core → (iii) magnetic carbon → (iv) carbonized magnetic carbon → (v) magnetic carbonaceous acid (catalyst). Detailed steps are described below:

#### 2.2.1. Magnetic core (Fe/C) by hydrothermal precipitation and pyrolysis

Aqueous solution (300 mL) of FeCl<sub>3</sub>·6H<sub>2</sub>O (81.1 g), glucose (45.75 g) and solid urea (30.0 g) were loaded into an autoclave lined with ZrO<sub>2</sub> (500 mL; FCFD05-30, Jianbang Chemical Mechanical Co., Ltd., Yantai, Shandong). The vessel was sealed and heated to 180 °C (heating rate: 3.8 °C/min) for 14 h hydrothermal reaction with stirring (500 rpm) [24]. After reactions  $[\text{CO}(\text{NH}_2)_2 + \text{H}_2\text{O} \rightarrow \text{NH}_3 + \text{CO}_2 + \text{NH}_4\text{OH}]$ ;  $\text{FeCl}_3 + \text{NH}_4\text{OH} \rightarrow \text{Fe}(\text{OH})_3 + \text{NH}_4\text{Cl}$ ;  $\text{Fe}(\text{OH})_3 \rightarrow \text{Fe}_2\text{O}_3 + \text{H}_2\text{O}$ , solid products were recovered and washed thoroughly with deionized water and ethanol several times until reaching neutral solution, then dried in a freeze dryer (PDU-1200, EYELA, Tokyo Rikakikai Co., Ltd.) at –47 °C for 24 h. The solid sample was heated to 700 °C (heating rate: 7.4 °C/min) for 1.5 h pyrolysis in a tubular furnace (SGL-1100, Shanghai Daheng Optics and Fine Mechanics Co., Ltd.) under nitrogen flowing (200 mL/min) to form carbon-based magnetic core (Fe/C) by dehydration and reduction  $[\text{Fe}(\text{OH})_3 \rightarrow \text{Fe}_2\text{O}_3 + \text{H}_2\text{O}; \text{Fe}_2\text{O}_3 + \text{C} \rightarrow \text{Fe}_3\text{O}_4/\text{Fe} + \text{CO}/\text{CO}_2]$ . It was found that the magnetic core had very weak magnetism after sulfonated [Ms of 0.43 Am<sup>2</sup>/kg with acid content of 1.67 mmol/g] due

**Table 1**

Comparison of acid content and magnetism of this work with other carbonaceous acid catalysts under different operation conditions.

| Sample  | Main raw materials  | Operation conditions  | Acid content (mmol/g)                       |                     | Magnetism (Am <sup>2</sup> /kg) | References |
|---|---|---|---|---------------------|---------------------------------|------------|
|   |   |   | NH <sub>3</sub> -TPD analysis               | Acid–base titration |                                 |            |
| SO <sub>3</sub> H–Fe/C                              | Glucose and FeCl <sub>3</sub>                                     | Hydrothermal precipitation: (180 °C, 14 h); pyrolysis: (700 °C, 1.5 h); sulfonation: (150 °C, H <sub>2</sub> SO <sub>4</sub> , 16 h)  | 1.67  | –                   | 0.43                            | This study |
| AC-600-SO <sub>3</sub> H@Fe/C                       | Glucose and FeCl <sub>3</sub>                                     | Hydrothermal precipitation: (180 °C, 14 h); pyrolysis: (700 °C, 1.5 h); hydrothermal coating: (180 °C, 14 h); pyrolysis: (600 °C, 1.5 h); sulfonation: (150 °C, H <sub>2</sub> SO <sub>4</sub> , 16 h)                    | 2.79 (1.0 <sup>a</sup> ; 3.7 <sup>b</sup> ) | –                   | 14.4                            | This study |
| Fe <sub>3</sub> O <sub>4</sub> @C–SO <sub>3</sub> H | Glucose and FeCl <sub>3</sub>                                     | Hydrothermal carbonization: (Glucose 180 °C, 14 h); desiccation: (40 °C, 12 h); sulfonation: (60 °C, H <sub>2</sub> SO <sub>4</sub> , 24 h)   | –   | 1.30                | 23                              | [24]       |
| MLC–SO <sub>3</sub> H                               | Enzymatic hydrolysis residue of corn stover and FeCl <sub>3</sub> | Mixture: (300 rpm, 5 h); impregnation: (65 °C, 12 h); pyrolysis: (400 °C, 1 h); sulfonation: (150 °C, H <sub>2</sub> SO <sub>4</sub> , 10 h)  | –   | 1.95                | –                               | [25]       |
| Sulfonated MCNAs                                    | Xylene and ferrocene  | Pyrolysis: (800 °C, the solution was injected by a syringe pump at a rate of 0.05 mL/min for 2 h with a flowrate of 60 sccm H <sub>2</sub> and 400 sccm Ar); sulfonation: (250 °C, H <sub>2</sub> SO <sub>4</sub> , 18 h) | 0.38  | –                   | 6.32 (before sulfonation)       | [26]       |

<sup>a</sup> By elemental analyzer.

<sup>b</sup> By EDX based on the calculation from the elemental composition of S.

to the dissolution of  $\text{Fe}_3\text{O}_4/\text{Fe}$ . So, it was re-coated with glucose in the next step.

### 2.2.2. Magnetic carbon (AC@Fe/C) by hydrothermal precipitation

The magnetic core was hydrothermally re-coated a carbonaceous layer with glucose to avoid leaching of  $\text{Fe}_3\text{O}_4/\text{Fe}$  during sulfonation. Fe/C powders (20 g), glucose (60 g) and  $\text{H}_2\text{O}$  (300 mL) were put into the above autoclave and heated to 180 °C for 14 h with stirring (500 rpm). After reactions, solid products were recovered by a permanent magnet (NeFeB, Ø37 mm × H18 mm), washed thoroughly with deionized water and ethanol several times until reaching neutral solution, dried in the freeze dryer at −47 °C for 24 h and an oven (WFO-710, EYELA, Tokyo Rikakikai Co., Ltd.) at 105 °C until reaching constant weight. The magnetic carbon was obtained and designated as AC@Fe/C.

### 2.2.3. Carbonized magnetic carbon (AC-T@Fe/C) by pyrolysis

In order to stabilize and restructure the magnetic carbon for sulfonation, it was heated to 400, 600 and 800 °C (heating rate: 4.1, 6.3 and 8.6 °C/min) for 1.5 h pyrolysis under nitrogen flowing (200 mL/min) in the tubular furnace to form carbonized magnetic carbons (designated as AC-T@Fe/C, T is pyrolysis temperature of 400, 600 and 800 °C) for sulfonation.

### 2.2.4. Magnetic carbonaceous acid (AC-T- $\text{SO}_3\text{H}$ @Fe/C) by sulfonation

The carbonized magnetic carbon (AC-T@Fe/C) particles (10.0 g) and concentrated  $\text{H}_2\text{SO}_4$  (98%, 200 mL) were added in a three-neck flask (500 mL) in oil bath (150 °C) for 16 h under nitrogen flowing (100 mL/min). The sulfonated samples were washed repeatedly with hot distilled water (80 °C) until reaching neutral solution, and hydrothermally pretreated at 200 °C (heating rate: 6 °C/min) for 3 h to remove  $\text{SO}_4^{2-}$  ions in the autoclave. After washed and dried in the freeze dryer at −47 °C for 24 h and the oven at 105 °C until reaching constant weight, the obtained catalysts (designated as AC-T- $\text{SO}_3\text{H}$ @Fe/C) were ground and sieved by 200-mesh for biodiesel production.

## 2.3. Characterization

Synthesized carbonaceous particles (Fe/C, AC@Fe/C and AC-T@Fe/C) before and after sulfonation were analyzed by X-ray diffraction (XRD; Rigaku Rotaflex RAD-C, Tokyo) using a Cu K $\alpha$  radiation source, and their morphologies were examined using scanning electron microscope (SEM; ZEISS EVO LS10, Cambridge, UK). Ms of samples was measured by a vibrating sample magnetometer (VSM; HH-15, Nanjing Nanda Instrument Plant, Jiangsu). Specific surface area and pore volume of samples were determined by Bruner Emmett and Teller (BET) method (Tristar II 3020, Micromeritics Instrument Co., Ltd., Northcross, GA). In the analysis, samples were degassed at 200 °C for 3 h and nitrogen with relative pressure of 0.05–0.985 was applied. The functional groups of catalysts were detected by Fourier transform-infrared spectroscopy (FT-IR; Nicolet iS10, Thermo Fisher Scientific Co., Ltd., Waltham, MA) over the range from 400 to 4000  $\text{cm}^{-1}$  with a resolution of 0.4–4  $\text{cm}^{-1}$  using the standard KBr disk method. Ammonia temperature programmed desorption ( $\text{NH}_3$ -TPD; Chemisorption analyzer, Quantachrome Instruments, Boynton Beach, FL) was used to assess their total acid density. In TPD analysis, sample (50–100 mg) was preheated to 400 °C at a heating rate of 5 °C/min to stabilize the catalyst and cooled to 50 °C exposed with He flowing (85 mL/min), and absorbed  $\text{NH}_3$  by flushing  $\text{NH}_3$  gas (10%  $\text{NH}_3$  and 90% He, 85 mL/min) for 60 min. The sample was subsequently desorbed by heating to 400 °C at a heating rate of 5 °C/min and kept for 60–90 min with He flowing (85 mL/min). Four different volumes (0.5, 1, 1.5, 2 mL) of a standard  $\text{NH}_3$  gas (10%  $\text{NH}_3$  and 90% He) were used to calibrate total acid density. Thermal stability

of catalysts (about 5 mg) was examined by thermo-gravimetric analysis (TGA; TA Q500 HiRes, T.A. Instruments, New Castle, DE). Temperature was ramped from 25 to 800 °C at 5 °C/min for data collection under He flowing (50 mL/min). Elemental compositions of catalysts were analyzed using an elemental analyzer (Vario EL III CHNS, Elementar Analysensysteme GmbH, Hanau, Germany). Synthesized particles, catalysts and biodiesel after carbonization were also analyzed to evaluate their elemental compositions or contaminants from catalysts by Energy-dispersive X-ray spectrometry (EDX; Quanta 200, Hillsboro, OR). It should be noted that the EDX data for elemental percentages are higher than actual values since H is not detectable and included.

## 2.4. Biodiesel production and analysis

Catalytic esterification and transesterification of crude *Jatropha* oil (about 18.6 g or 0.02 mol) without pretreatment with dehydrated methanol (methanol/oil molar ratio of 6/1–30/1) and catalyst (2.5–12.5 wt% of oil) were conducted in an autoclave with 50-mL quartz cup and 9.6-mL dead volume (YZPR-50, YanZheng Shanghai Experimental Instrument Co., Ltd.). The autoclave was sealed and pressurized with nitrogen to initial pressure of 2 MPa to avoid methanol evaporation to the dead volume at high temperature, and heated to 180–220 °C within 20–40 min under 750 rpm stirring. The actual reaction pressure in the reactor was 4.0 MPa at 180 °C and 6.5 MPa at 220 °C, that is much higher than the saturated methanol vapor pressure at corresponding temperature (e.g., 2.7 MPa at 180 °C and 5.8 MPa at 220 °C [28]). After reactions, catalyst was attracted on the wall of quartz cup by a magnet for 0.5–1 h (Fig. 1b) and liquid products were removed to a flask. The catalyst was washed by ethanol (20 mL) under magnetic stirring thoroughly (30 min) for 3–5 times, and dried at 105 °C until reaching a consistent weight. Recovery rate of catalyst was defined as:

$$\text{Recovery rate (wt\%)} = \frac{\text{mass of recovered catalyst}}{\text{mass of fresh catalyst}} \times 100\% \quad (1)$$

Crude biodiesel in the flask at upper layer was filtered (pore size 0.22  $\mu\text{m}$ ) and analyzed by Gas Chromatography (GC; GC-2014, Shimadzu, Kyoto) with a capillary column of Rtx-Wax (30 m × Ø0.25 mm × 0.25  $\mu\text{m}$ ) under analytical conditions of column temperature 220 °C, injector temperature 260 °C, detector temperature 280 °C, carrier gas (He) with a flow rate 1 mL/min and split ratio 40/1. HDAM ( $\text{C}_{17:0}$ ) was used as internal standard for quantitative analysis, according to the weights and GC peak areas of crude biodiesel and HDAM, biodiesel yield was calculated by equation:

$$\begin{aligned} \text{Biodiesel yield (wt\%)} = \{ & [(A_{\text{C}_{16:0}}/f_{\text{C}_{16:0}} + A_{\text{C}_{16:1}}/f_{\text{C}_{16:1}} + A_{\text{C}_{18:0}}/f_{\text{C}_{18:0}} \\ & + A_{\text{C}_{18:1}}/f_{\text{C}_{18:1}} + A_{\text{C}_{18:2}}/f_{\text{C}_{18:2}} + A_{\text{C}_{18:3}}/f_{\text{C}_{18:3}} \\ & + A_{\text{C}_{\text{others}}})/A_{\text{C}_{17:0}}] \times \text{weight of C}_{17:0} \} / \\ & \times (\text{weight of crude biodiesel}) \times 100\% \quad (2) \end{aligned}$$

where  $f_{\text{C}_n}$  (1.014, 1.023, 1.076, 1.038, 1.019 and 0.926) ( $n = 16:0, 16:1, 18:0, 18:1, 18:2, 18:3$ ) is the relative response factor of six standard methyl esters [palmitate ( $\text{C}_{16:0}$ ), linolenate ( $\text{C}_{16:1}$ ), stearate ( $\text{C}_{18:0}$ ), oleate ( $\text{C}_{18:1}$ ), linoleate ( $\text{C}_{18:2}$ ) and linolenate ( $\text{C}_{18:3}$ )] to that of HDAM. It was separately calibrated for each GC peak in our previous work [29].  $A_{\text{C}_n}$  is area for  $\text{C}_n$  peak.  $A_{\text{C}_{\text{others}}}$  is area for other components except  $A_{\text{C}_n}$ .

## 3. Results and discussion

Photos for biodiesel production and catalyst separation in reaction quartz cup are showed in Fig. 1. Analytical results of XRD, VSM, SEM, BET, FT-IR,  $\text{NH}_3$ -TPD and TGA for synthesized particles and

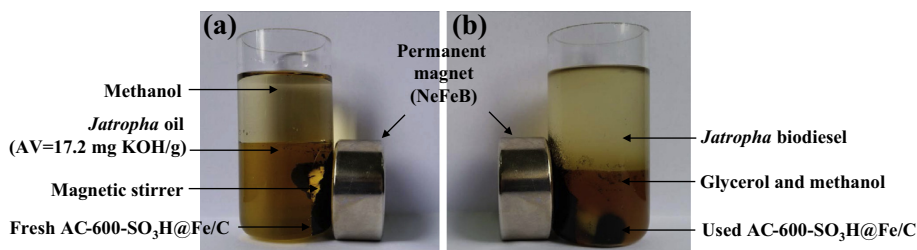


Fig. 1. Biodiesel production and catalyst separation in reaction quartz cup: (a) before and (b) after reaction.

catalysts are presented in Figs. 2–8, respectively. Table 1 compares acid content and magnetism of magnetic solid acids of this work with previous studies. Particle size of iron and iron oxides was calculated based on XRD data and listed in Table 2. Single-factor optimization, catalyst activity at different carbonized temperatures and catalyst cycles for biodiesel production from *Jatropa* oil with high AV (17.2 mg KOH/g) are given in Figs. 9–11. Element analysis of carbonized magnetic carbon (AC-600@Fe/C) and magnetic carbonaceous acid (AC-600-SO<sub>3</sub>H@Fe/C) by EDX is demonstrated in supplemental materials (Fig. S1). Recycled catalysts were also analyzed by NH<sub>3</sub>-TPD and results are illustrated in Figs. S2 and S3. EDX spectra of carbonized biodiesel (10 mL) catalyzed by magnetic carbonaceous acid (AC-600-SO<sub>3</sub>H@Fe/C) are given in Fig. S4.

### 3.1. Characterization

#### 3.1.1. XRD

In Fig. 2, the crystalline phases of Fe, Fe<sub>3</sub>O<sub>4</sub>, Fe<sub>3</sub>C, Fe<sub>2</sub>O<sub>3</sub> and aromatic carbon sheets are identified as compared with the cards from Joint Committee on Powder Diffraction Standards (JCPDS: 06-0696, 89-2355, 72-1110 and 39-1346) and Ref. [30]. The average particle size of Fe<sub>3</sub>O<sub>4</sub> and Fe was calculated by Scherer equation [31]:  $D_c = K\lambda/(\beta\cos\theta)$  (where  $D_c$  is the average particle size;  $K$  (0.89) is the Scherer constant;  $\lambda$  (0.1541 nm) is the X-ray wavelength of Cu K $\alpha$  radiation;  $\beta$  is full-width at half-maximum;  $\theta$  is the diffraction angle of the XRD reflection) (Table 2).

Fig. 2A shows that Fe/C and AC@Fe/C carbonaceous particles have well-crystallized Fe<sub>3</sub>O<sub>4</sub> and Fe structures with characteristic and symmetric reflections, but the peak intensity of AC@Fe/C is much weaker due to a carbon layer coated. Fe<sub>3</sub>O<sub>4</sub> particles have the same size in Fe/C and AC@Fe/C (29.5 nm) samples, but Fe particle size decreased from 53.1 nm in Fe/C to 42.5 nm in AC@Fe/C after coated hydrothermally.

In Fig. 2B, after carbonized at 400 °C, Fe<sub>3</sub>O<sub>4</sub> and Fe crystals (in AC-400@Fe/C) changed little in characteristic reflections and particle size (Fig. 2B-a vs. Fig. 2A-b). As carbonized temperature rose from 400 to 600 and 800 °C (Fig. 2B-a, b and c), the diffraction peaks of Fe<sub>3</sub>O<sub>4</sub> particles disappeared gradually, but Fe particle size increased from 42.5 to 106.3 nm then dipped to 70.8 nm. When temperature increased, Fe<sub>3</sub>O<sub>4</sub> was reduced to Fe by carbon [Fe<sub>3</sub>O<sub>4</sub> + C → Fe + CO<sub>2</sub>/CO↑] at 600 °C [32], and further to Fe<sub>3</sub>C particles [Fe + C → Fe<sub>3</sub>C] at 800 °C [33].

In Fig. 2C, after sulfonated, XRD spectra of magnetic carbonaceous acids (AC-T-SO<sub>3</sub>H@Fe/C) change dramatically. Only a strong peak (for aromatic carbon sheet) remains if AC@Fe/C carbonized at 400 °C. At higher temperatures (Fig. 2C-b, 600 °C; Fig. 2C-c, 800 °C), additional Fe and Fe<sub>2</sub>O<sub>3</sub> peaks appear because in concentrated H<sub>2</sub>SO<sub>4</sub> solution, Fe was coated with dense oxidized Fe<sub>2</sub>O<sub>3</sub> film [Fe + H<sub>2</sub>SO<sub>4</sub> → Fe<sub>2</sub>O<sub>3</sub> + H<sub>2</sub>O + SO<sub>2</sub>↑] that protected it from further corrosion. But, most of Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>C particles dissolved in H<sub>2</sub>SO<sub>4</sub> solution (Fig. 2B vs. 2C). All sulfonated catalysts exhibit a broad and strong diffraction peak (at 2-Theta = 20–30°) for aromatic carbon sheets [30] due to the presence of amorphous carbons oriented in a random fashion [34]. But, the peak intensity

declines gradually as the carbonized temperature rises from 400 to 800 °C (Fig. 2C-a, b and c). This may be due to that the carbonized magnetic carbons at low temperature (e.g., AC-400@Fe/C) with rich hydrogen and oxygen elements were easier to build aromatic carbon sheet structures when sulfonated in concentrated H<sub>2</sub>SO<sub>4</sub> [34]. But, a portion of aromatic carbon sheet structures were formed at 800 °C (Fig. 2B-c) and inhibited concentrated H<sub>2</sub>SO<sub>4</sub> to corrode carbon skeleton further [35].

#### 3.1.2. VSM

Fig. 3A shows that Ms of the carbonized magnetic carbons is 23.5, 98.9 and 73.7 Am<sup>2</sup>/kg at carbonized temperature of 400, 600 and 800 °C, respectively. This is because that Fe<sub>3</sub>O<sub>4</sub> formed at 400 °C changed to Fe at 600 °C, and to Fe<sub>3</sub>C at 800 °C as discussed above while Fe/Fe<sub>3</sub>C has stronger magnetism than Fe<sub>3</sub>O<sub>4</sub> [36] and Fe<sub>3</sub>C has a lower Ms value than Fe [33]. So, AC-600@Fe/C has the strongest magnetism. After sulfonation, Ms decreased to 2.6, 14.4 and 11.1 Am<sup>2</sup>/kg at carbonized temperature of 400, 600 and 800 °C, respectively (Fig. 3B) because of the dissolution of Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>C in concentrated H<sub>2</sub>SO<sub>4</sub> solution. AC-600-SO<sub>3</sub>H@Fe/C catalyst has the strongest magnetism because it contains the highest Fe (Fig. 2C-b vs. a and c).

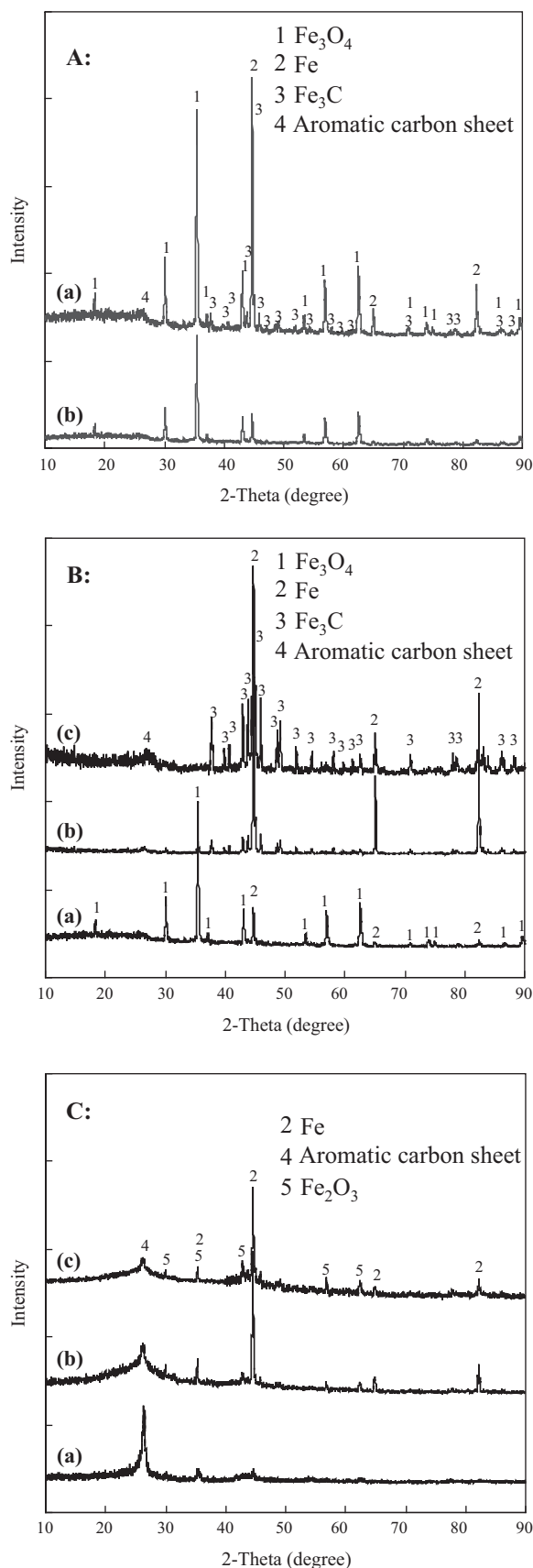
#### 3.1.3. SEM

In Fig. 4A-a, the magnetic core (Fe/C) is composed of porous particles (10–30 μm) agglomerated with tiny rough particles (<10 μm). After hydrothermally coated, they slightly grew to bigger particles agglomerated with smooth spheres (Fig. 4A-b). Little changed after the magnetic carbon (AC@Fe/C) carbonized at 400–800 °C (Fig. 4B). However, after sulfonation, the morphologies of magnetic carbonaceous acids (AC-T-SO<sub>3</sub>H@Fe/C) changed dramatically for the carbonized magnetic carbon (AC-T@Fe/C) at low temperatures (400 and 600 °C). For example, catalyst AC-400-SO<sub>3</sub>H@Fe/C became porous particles (Fig. 4C-a) from smooth spheres (Fig. 4B-a), but some spherical particles still remained for AC-600-SO<sub>3</sub>H@Fe/C at higher carbonized temperature of 600 °C (Fig. 4C-b vs. Fig. 4B-b). When temperature rose to 800 °C, little morphology changed for AC-800-SO<sub>3</sub>H@Fe/C catalyst (Fig. 4C-c vs. Fig. 4C-c). High carbonized temperature of 800 °C resulted in stable char structure to resist H<sub>2</sub>SO<sub>4</sub> attack. At low pyrolysis temperatures of 400 and 600 °C, the carbon framework was flexible [35] to be corroded and dehydrated by H<sub>2</sub>SO<sub>4</sub> during the sulfonation process.

#### 3.1.4. BET

Nitrogen adsorption–desorption isotherms are given in Fig. 5. The carbonized magnetic carbon at 400 °C (AC-400@Fe/C) exhibits a very low adsorption capacity for nitrogen without clear hysteresis loop with pore volume of only 0.0063 cm<sup>3</sup>/g and specific surface area of 4.28 m<sup>2</sup>/g (Fig. 5A-a). It can be regarded it as nonporous amorphous carbon due to incomplete carbonization at 400 °C, and a large number of hydrogen and oxygen atoms still remained without the formation of porous structure [35]. As carbonized temperature increased to 600 °C (Fig. 5A-b), specific surface area rose





**Fig. 2.** XRD patterns of (A) magnetic core (a: Fe/C) and magnetic carbon (b: AC@Fe/C), (B) carbonized magnetic carbon (AC-T@Fe/C), and (C) magnetic carbonaceous acid (AC-T-SO<sub>3</sub>H@Fe/C) (a:  $T = 400$ ; b:  $T = 600$ ; and c:  $T = 800$ ).

to 36.5 m<sup>2</sup>/g with larger pore volume (0.03 cm<sup>3</sup>/g) due to numerous micro pore formation by removal of hydrogen and oxygen as volatile gases at 600 °C [37,38]. The generation of CO<sub>2</sub>/CO in the reduction of Fe<sub>3</sub>O<sub>4</sub> by carbon helped to create porous structures in AC-600@Fe/C [25]. At higher temperature of 800 °C (Fig. 5A-c), specific surface area jumped further to 56.3 m<sup>2</sup>/g with pore volume of 0.12 cm<sup>3</sup>/g due to deep degree pyrolysis and reduction reaction.

After sulfonation, both specific surface area and pore volume of magnetic carbonaceous acids (AC-T-SO<sub>3</sub>H@Fe/C) rose with values of (218.5 m<sup>2</sup>/g and 0.81 cm<sup>3</sup>/g vs. 4.28 m<sup>2</sup>/g and 0.0063 cm<sup>3</sup>/g) at 400 °C, (88.9 m<sup>2</sup>/g and 0.14 cm<sup>3</sup>/g vs. 36.5 m<sup>2</sup>/g and 0.03 cm<sup>3</sup>/g) at 600 °C, and (57.3 m<sup>2</sup>/g and 0.16 cm<sup>3</sup>/g vs. 56.3 m<sup>2</sup>/g and 0.12 cm<sup>3</sup>/g) at 800 °C, respectively (Fig. 5B vs. A). The sharp increases for the sulfonated carbonaceous acid carbonized at 400 °C (but only slight rise at 800 °C) are due to that the unstable structure of carbonized magnetic carbon (AC-400@Fe/C) after incomplete pyrolysis was easily corroded and dehydrated by H<sub>2</sub>SO<sub>4</sub> sulfonation to form micro porous particles with high surface area. On the other hand, the dissolution of Fe<sub>3</sub>O<sub>4</sub> and Fe<sub>3</sub>C particles also contributed the rising.

### 3.1.5. FT-IR

Fig. 6A shows the FT-IR spectra of magnetic carbons (AC-T@Fe/C) after carbonized at 400, 600 and 800 °C, respectively. All samples have absorptions at 1610 and 3460 cm<sup>-1</sup> from O—H and C=O stretching vibration in phenolic —OH and —COOH groups generated during carbonization [25]. But, a strong absorption (Fig. 6A-a) at 560 cm<sup>-1</sup> for AC-400@Fe/C from Fe—O stretching vibration in Fe<sub>3</sub>O<sub>4</sub> [25] gradually disappeared due to its reduction to Fe and Fe<sub>3</sub>C at high temperatures of 600 and 800 °C (Fig. 6A-b, c) as discussed in the above Section 3.1.1 XRD (Fig. 2B).

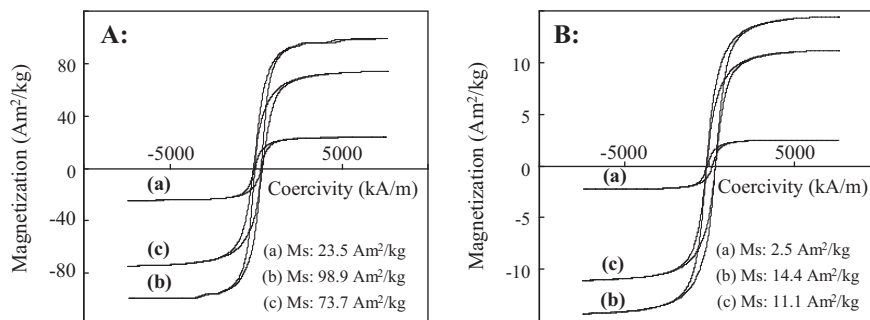
After sulfonation (Fig. 6B), all samples have absorptions at 1060 and 1180 cm<sup>-1</sup> from C—O—S and O=S=O stretching vibration in —SO<sub>3</sub>H groups [25]. The absorption at 1640 cm<sup>-1</sup> is from C=C stretching vibration in aromatic carbons. The absorption at 560 cm<sup>-1</sup> for Fe—O stretching vibration in AC-400-SO<sub>3</sub>H@Fe/C disappeared (Fig. 6B-a), but appeared in AC-600-SO<sub>3</sub>H@Fe/C and AC-800-SO<sub>3</sub>H@Fe/C. This is because that Fe<sub>3</sub>O<sub>4</sub> in AC-400@Fe/C dissolved during sulfonation, but Fe<sub>2</sub>O<sub>3</sub> was formed from Fe in the catalysts carbonized at 600 and 800 °C by oxidation of Fe in concentrated H<sub>2</sub>SO<sub>4</sub> as confirmed by XRD analysis (Fig. 2C).

AC-600@Fe/C before and after sulfonation was analyzed by EDX (Fig. S1), the spectra revealed that S content dramatically increased from <0.3 wt% to <12.2 wt% after sulfonation, indicating that —SO<sub>3</sub>H groups were successfully incorporated into the carbonized magnetic carbon. The trace amount of S before sulfonation for AC-600@Fe/C was possibly from the contaminated S compounds remained in autoclave.

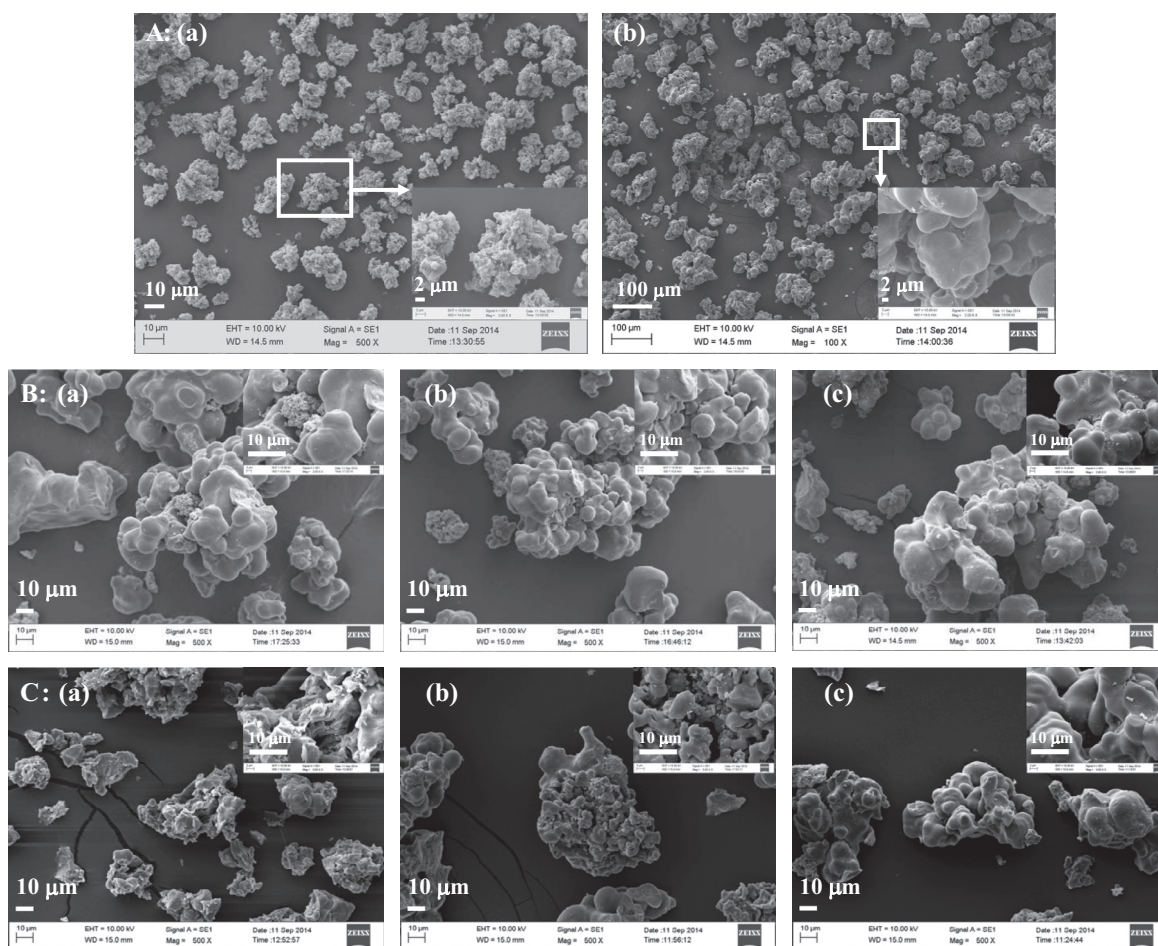
### 3.1.6. TPD

Total acid density of magnetic carbonaceous acids (AC-T-SO<sub>3</sub>H@Fe/C) was determined by NH<sub>3</sub>-TPD analysis (Fig. 7).

For carbonized magnetic carbons (Fig. 7A), a major desorption peak at 135 °C appeared for AC-400@Fe/C (total acid density 0.12 mmol/g) from incompletely formed carbon sheets with weak acid sites (—OH and —COOH) [17]. Total acid density rose to 0.27 mmol/g for AC-600@Fe/C when carbonized temperature grew to 600 °C due to its larger specific surface area and pore volume (36.5 m<sup>2</sup>/g vs. 4.28 m<sup>2</sup>/g) and (0.03 cm<sup>3</sup>/g vs. 0.0063 cm<sup>3</sup>/g) (Fig. 7A-b vs. a) with more acid sites exposed on the surface and inner wall [39,40]. However, total acid density dropped to only 0.05 mmol/g for AC-800@Fe/C because less acid sites or hydrogen and oxygen elements remained at 800 °C [22,37] even though it had high specific surface area and pore volume.



**Fig. 3.** Hysteresis loops of (A) carbonized magnetic carbon (AC-T@Fe/C) and (B) magnetic carbonaceous acid (AC-T-SO<sub>3</sub>H@Fe/C) (a:  $T = 400$ ; b:  $T = 600$ ; and c:  $T = 800$ ).

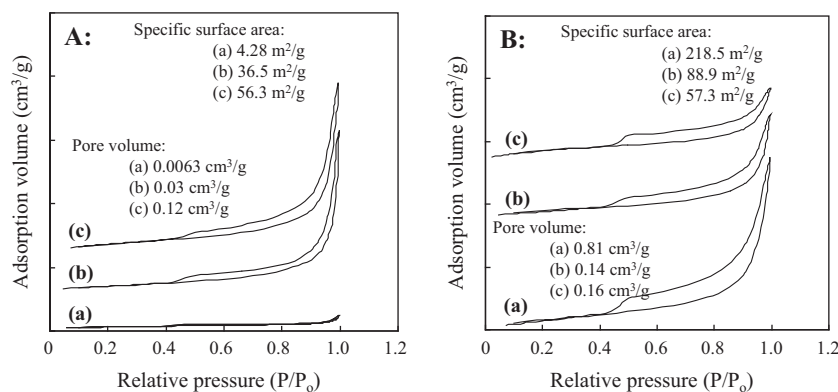


**Fig. 4.** SEM images of (A) magnetic core (a: Fe/C) and magnetic carbon (b: AC@Fe/C), (B) carbonized magnetic carbon (AC-T@Fe/C), and (C) magnetic carbonaceous acid (AC-T-SO<sub>3</sub>H@Fe/C) (a:  $T = 400$ ; b:  $T = 600$ ; and c:  $T = 800$ ).

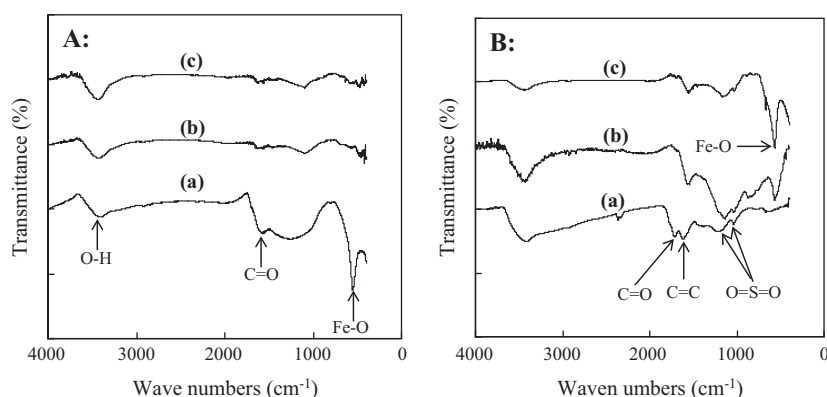
After sulfonation (Fig. 7B), 2–3 major desorption peaks are observed at 50–400 °C for the catalysts, and total acid density rises more than 10 times [(3.26 vs. 0.12 mmol/g) at 400 °C, (2.79 vs. 0.27 mmol/g) at 600 °C, (1.24 vs. 0.05 mmol/g) at 800 °C] because of the presence of active group ( $-\text{SO}_3\text{H}$ ). The sulfonated carbonaceous catalysts have high total acid density when they were carbonized at low temperatures (400 and 600 °C), but have a very low value at 800 °C. This is because many hydrogen and oxygen atoms still remained in the catalysts when carbonized at 400 and 600 °C, to attach  $-\text{SO}_3\text{H}$  group [37] but the formed aromatic carbon sheet at 800 °C in AC-800@Fe/C (Fig. 2B-c) inhibited the attachment [35]. Elemental compositions of AC-600-SO<sub>3</sub>H@Fe/C were also analyzed and showed an increase in S content (3.2 S,

63.6 C, 2.3 H and 1.1 wt% N vs. 0.2 S, 59.1 C, 2.0 H and 1.8 wt% N before sulfonation) with its sulfuric acid density ( $-\text{SO}_3\text{H}$ ) increased from 0.06 to 1.0 mmol/g calculated based on S content. EDX spectrum reveals a high S content of 12.2% (Fig. S1b), if including 2% H, the S content is about 12% (or 3.7 mmol/g sulfuric acid density) that is much higher than 3.2% obtained by elemental analyzer. These results demonstrate that the re-coated carbon layer on the surface has a much higher acid density because it has more functional groups and chance to bond  $-\text{SO}_3\text{H}$  than the magnetic core.

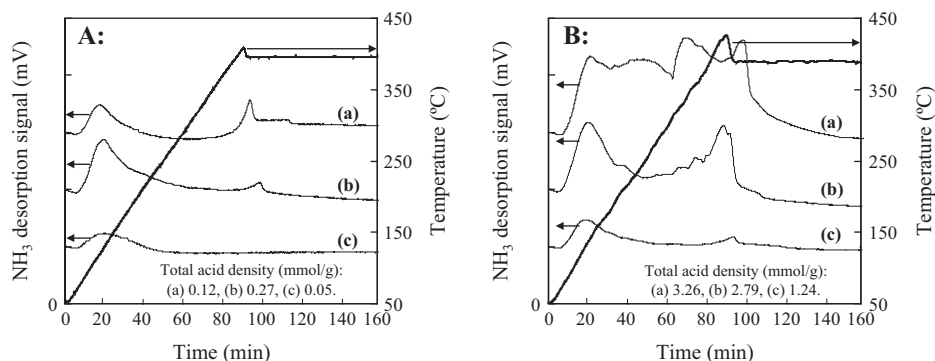
Since AC-600-SO<sub>3</sub>H@Fe/C catalyst has the strongest magnetism (Ms: 14.4 Am<sup>2</sup>/kg) with high total acid density (2.79 mmol/g), it is selected for biodiesel production in next section. As compared to other magnetic carbonaceous acids in previous works (Table 1),



**Fig. 5.** Nitrogen adsorption/desorption isotherms of (A) carbonized magnetic carbon (AC-T@Fe/C) and (B) magnetic carbonaceous acid (AC-T-SO<sub>3</sub>H@Fe/C) (a:  $T = 400$ ; b:  $T = 600$ ; and c:  $T = 800$ ).



**Fig. 6.** FT-IR spectra of (A) carbonized magnetic carbon (AC-T@Fe/C) and (B) magnetic carbonaceous acid (AC-T-SO<sub>3</sub>H@Fe/C) (a:  $T = 400$ ; b:  $T = 600$ ; and c:  $T = 800$ ).



**Fig. 7.** NH<sub>3</sub>-TPD curves of (A) carbonized magnetic carbon (AC-T@Fe/C) and (B) magnetic carbonaceous acid (AC-T-SO<sub>3</sub>H@Fe/C) (a:  $T = 400$ ; b:  $T = 600$ ; and c:  $T = 800$ ).

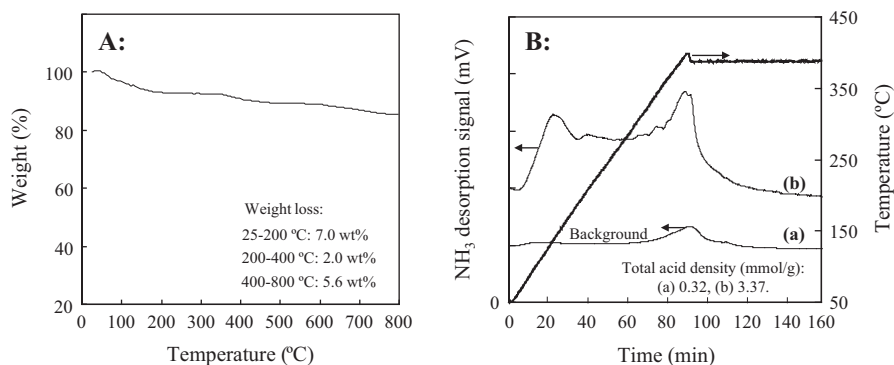
such as Fe<sub>3</sub>O<sub>4</sub>@C-SO<sub>3</sub>H [24], MLC-SO<sub>3</sub>H [25] and sulfonated MCNAs [26], AC-600-SO<sub>3</sub>H@Fe/C catalyst has the highest acid content (2.79 vs. 1.3, 1.95 and 0.38 mmol/g) with strong magnetism. Even though, Fe<sub>3</sub>O<sub>4</sub>@C-SO<sub>3</sub>H has the higher Ms (23 Am<sup>2</sup>/kg) but its acid content is too low (1.3 mmol/g) because of its low sulfonated temperature than AC-600-SO<sub>3</sub>H@Fe/C (60 °C vs. 150 °C).

In the above TPD results, catalysts were stabilized via thermal pretreatment by heating to 400 °C with He flowing, they may be decomposed before NH<sub>3</sub> absorption. Therefore, thermal stability of AC-600-SO<sub>3</sub>H@Fe/C catalyst was analyzed by TGA. In Fig. 8A, it is found that a minor weight loss (about 7.0 wt%) at 25–200 °C from the release of water and gases [34], and a very slight thermal decomposition at 200–400 °C (2.0 wt% of weight loss) probably

from polycyclic aromatic hydrocarbons bonded to sulfuric groups. So, an additional TPD analysis was conducted for AC-600-SO<sub>3</sub>H@Fe/C without thermal pretreatment (Fig. 8B), a slight higher total acid density (3.05 vs. 2.79 mmol/g) was obtained (datum of 0.32 for a blank run without adsorption of NH<sub>3</sub> was subtracted, Fig. 8B-a). The total acid density data analyzed in this work may present smaller slightly.

### 3.2. *Jatropha* biodiesel production with AC-600-SO<sub>3</sub>H@Fe/C

Variables of catalyst dosage (2.5–12.5 wt% of oil), methanol/oil molar ratio (6/1–30/1), reaction temperature (180–220 °C) and reaction time (2.5–12.5 h, excluding heating and cooling times)



**Fig. 8.** (A) TGA and (B) NH<sub>3</sub>-TPD curves of AC-600-SO<sub>3</sub>H@Fe/C catalyst without thermal pretreatment at 400 °C (a: a blank run without adsorption of NH<sub>3</sub> as background).

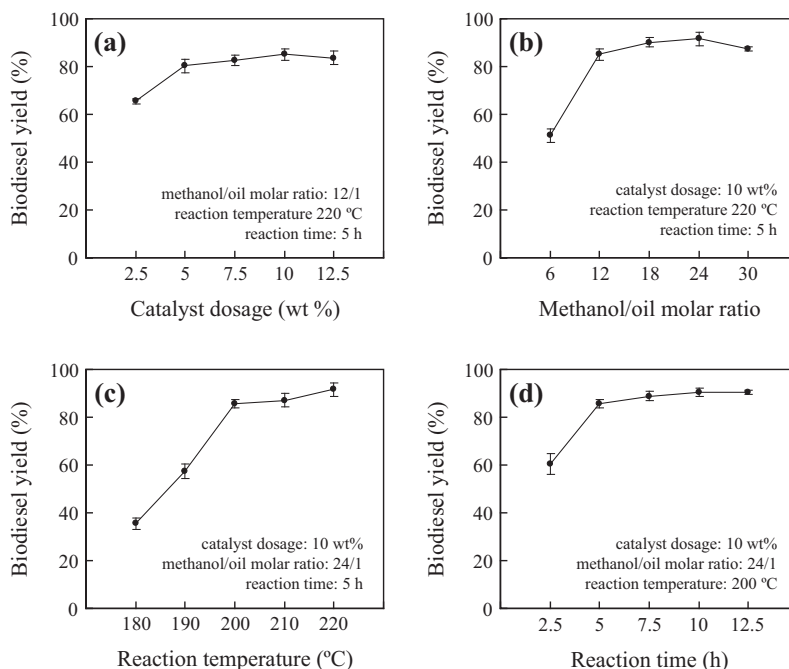
**Table 2**  
Average particle size of Fe<sub>3</sub>O<sub>4</sub> and Fe crystals calculated by Scherer equation:  $D_c = K\lambda/(\beta\cos\theta)$  ( $\theta$  for Fe<sub>3</sub>O<sub>4</sub> is  $35.46^\circ/2 \times 3.14/180 = 0.31$ , and for Fe is  $44.74^\circ/2 \times 3.14/180 = 0.39$ ).

| No.       | Sample      | Crystalline phase              | $\beta$                               | Particle size (nm) |
|-----------|-------------|--------------------------------|---------------------------------------|--------------------|
| Fig. 2A-a | Fe/C        | Fe <sub>3</sub> O <sub>4</sub> | $0.28^\circ \times 3.14/180 = 0.0049$ | 29.5               |
|           |             | Fe                             | $0.16^\circ \times 3.14/180 = 0.0035$ | 53.1               |
| Fig. 2A-b | AC@Fe/C     | Fe <sub>3</sub> O <sub>4</sub> | $0.28^\circ \times 3.14/180 = 0.0049$ | 29.5               |
|           |             | Fe                             | $0.2^\circ \times 3.14/180 = 0.0035$  | 42.5               |
| Fig. 2B-a | AC-400@Fe/C | Fe <sub>3</sub> O <sub>4</sub> | $0.28^\circ \times 3.14/180 = 0.0049$ | 29.5               |
|           |             | Fe                             | $0.2^\circ \times 3.14/180 = 0.0035$  | 42.5               |
| Fig. 2B-b | AC-600@Fe/C | Fe <sub>3</sub> O <sub>4</sub> | –                                     | –                  |
|           |             | Fe                             | $0.12^\circ \times 3.14/180 = 0.0021$ | 106.3              |
| Fig. 2B-c | AC-800@Fe/C | Fe <sub>3</sub> O <sub>4</sub> | –                                     | –                  |
|           |             | Fe                             | $0.08^\circ \times 3.14/180 = 0.0014$ | 70.8               |

were studied for the esterification and transesterification of *Jatropha* oil with high AV (17.2 mg KOH/g) to biodiesel by single factor test. Two repeated experiments were done for each run and the reported biodiesel yields were averaged data with standard deviation ( $\sigma$ ) of 0.8–4.2% (Fig. 9). The initial conditions set below for optimization are referred to the previous results (catalyst of 5 wt%, methanol/oil molar ratio of 12/1, reaction temperature of 220 °C and reaction time of 5 h) [23].

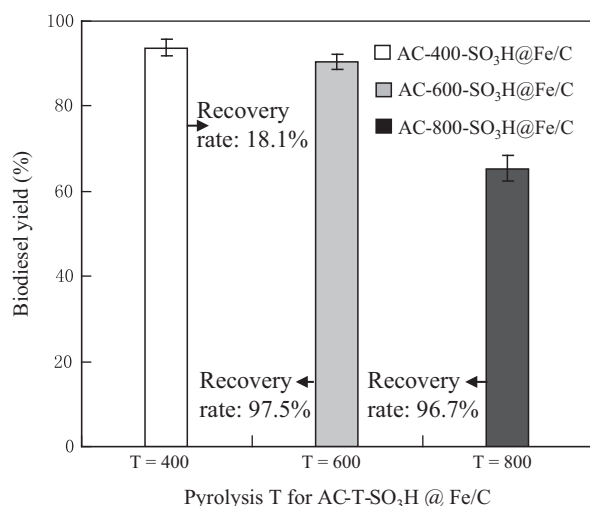
### 3.2.1. Catalyst dosage

Catalyst from 2.5 wt% to 12.5 wt% was applied for biodiesel production under conditions of 220 °C for 5 h with 12/1 methanol/oil molar ratio. In Fig. 9a, biodiesel yield jumped sharply from 65.5% to 80.3% as catalyst rose from 2.5 wt% to 5 wt%, and increased gradually to the highest yield of 85.1% at 10 wt% catalyst. However, as catalyst grew further from 10 wt% to 12.5 wt%, biodiesel yield dropped slightly from 85.1% to 83.6%. This was possibly due to



**Fig. 9.** Single-factor optimization of biodiesel production from *Jatropha* oil (AV = 17.2 mg KOH/g) with AC-600-SO<sub>3</sub>H@Fe/C magnetic acid catalyst: (a) catalyst dosage, (b) methanol/oil molar ratio, (c) reaction temperature, and (d) reaction time.





**Fig. 10.** *Jatropha* biodiesel yield changed with pyrolysis temperature for AC-T-SO<sub>3</sub>H@Fe/C catalyst (Reaction conditions: 200 °C for 10 h with 24/1 methanol/oil molar ratio and 10 wt% catalyst).

the difficult mixing of liquid reactants with high concentration of magnetic carbonaceous catalyst under magnetic stirring. So, 10 wt% catalyst is selected as the best value for the next experiments.

### 3.2.2. Methanol/oil molar ratio

Theoretical methanol/oil molar ratio for the transesterification of triglycerides is 3/1. High methanol/oil molar ratio from 6/1 to 30/1 was required in this work under 220 °C for 5 h with 10 wt% catalyst because of the evaporation of methanol to the dead volume of the autoclave at high temperature (Fig. 9b). When methanol/oil molar ratio grew from 6/1 to 12/1, biodiesel yield rose sharply from 51.1% to 85.1%, and gradually increased to 90.2% and the maximum of 91.6% at molar ratio of 18/1 and 24/1, respectively. But, the yield dropped slightly to 87.5% at molar ratio of 30/1 owing to the relative low concentration of catalyst in the reaction system caused by excess methanol. So, 24/1 methanol/oil molar ratio is selected as the best value for the following experiments.

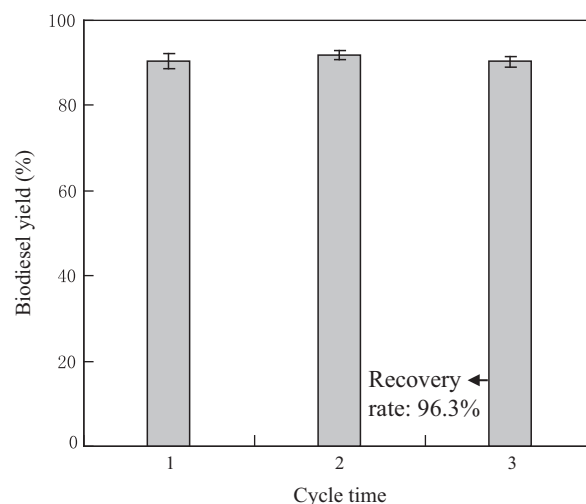
### 3.2.3. Reaction temperature

Five different temperatures from 180 to 220 °C were selected for biodiesel production with 10 wt% catalyst, 24/1 methanol/oil molar ratio and 5 h reaction time (Fig. 9c). A big increase in biodiesel yield (85.6% vs. 35.5%) occurred from 180 to 200 °C, and the yield rose slowly to 87.2% at 210 °C and 91.6% at 220 °C, respectively. High temperature resulted in high biodiesel yield, but the active group is easily leached. So, 200 °C is selected as the best value.

### 3.2.4. Reaction time

Reaction time from 2.5 to 12.5 h was chosen for biodiesel production under conditions of 10 wt% catalyst, 24/1 methanol/oil molar ratio and 200 °C temperature (Fig. 9d). When time rose from 2.5 to 5 h, biodiesel yield increased from 60.5% to 85.6% sharply, and gradually rose to 88.8%, 90.5% and 90.6% at 7.5, 10 and 12.5 h, respectively. Since little increased for biodiesel yield from 10 to 12.5 h, the best value for reaction time is selected as 10 h.

In conclusion, the best conditions for *Jatropha* biodiesel production with 90.5% biodiesel yield were selected as: 10 wt% catalyst, 24/1 methanol/oil molar ratio, 200 °C temperature and 10 h reaction time. Under the conditions, catalyst recovery and recycles are studied in next section.



**Fig. 11.** Catalyst (AC-600-SO<sub>3</sub>H@Fe/C) cycles for the *Jatropha* biodiesel production (Reaction conditions: 200 °C for 10 h with 24/1 methanol/oil molar ratio and 10 wt% catalyst).

### 3.2.5. Catalyst recovery and recycles

Under the above best conditions, the three synthesized catalysts (AC-T-SO<sub>3</sub>H@Fe/C; T = 400, 600 and 800) were tested to catalyze biodiesel production (Fig. 10). Biodiesel yields were 92.7%, 90.5% and 65.4% with catalysts carbonized at 400, 600 and 800 °C, that were corresponding to their total acid densities of 3.26, 2.79 and 1.24 mmol/g, respectively. After first-used, the catalysts (AC-T-SO<sub>3</sub>H@Fe/C; T = 400, 600 and 800) were recovered by a magnet with recovery rate of 18.1%, 97.5% and 96.7%, that was corresponding to their magnetisms (Ms) of 2.5, 14.4 and 11.1 Am<sup>2</sup>/kg, respectively. TPD analysis shows that total acid density was reduced to 2.17, 2.52 and 1.03 mmol/g for the first-used catalysts carbonized at 400, 600 and 800 °C, respectively (Fig. S2). These experimental results show that AC-600-SO<sub>3</sub>H@Fe/C is the best catalyst for *Jatropha* biodiesel production as we supposed before for its excellent performance in recovery rate and stability.

Recycle experiments were conducted for AC-600-SO<sub>3</sub>H@Fe/C catalyst (Fig. 11). Little biodiesel yield changed for three cycles (90.5%, 91.8%, 90.3%) with high catalyst recovery rate of 96.3% after 3 cycles due to only a slight reduction in total acid density (from 2.79 to 2.43 mmol/g) (Fig. S3).

Biodiesels from the three cycles were analyzed their AV by titration with values of 0.12, 0.09 and 0.13 mg KOH/g that are lower than the value (0.5 mg KOH/g) for US national standard [41]. The three biodiesels (10 mL) were carbonized at 700 °C, and analyzed by EDX and found they were composed of C and O (H undetectable) without any Fe and other elements contaminated from the catalyst in the three cycles (Fig. S4).

### 3.3. Applications

For biodiesel production from high AV cooking oil (12 mg KOH/g), Zhang et al. [42,43] compared two main conventional methods [one-step acid-catalyzed with H<sub>2</sub>SO<sub>4</sub> at 80 °C vs. two-step alkali-catalyzed after acid-pretreatment (esterification with H<sub>2</sub>SO<sub>4</sub> at 70 °C, and transesterification with NaOH at 60 °C) processes] on a commercial scale. Economic assessment and sensitivity analysis showed that the one-step process proved to be technically feasible with less complexity (such as without pretreatment unit for esterification reactor, glycerol washing tower and methanol recovery process) than the two-step process. So, one-step process is a competitive alternative to commercial biodiesel production by the alkali-catalyzed process (e.g., 644 vs. 884

\$/tonne of break-even price of biodiesel) [43]. However, liquid acid  $\text{H}_2\text{SO}_4$  is hard to recover and usually requires neutralization.

In this work, one-step process was also used to produce biodiesel in the presence of the synthesized magnetic carbonaceous acid directly from low-qualified oils with high AV (17.2 mg KOH/g) without pretreatment. After reactions, the biodiesel contains high fatty acid methyl esters (FAMES; 90–92% purity or biodiesel yield) and low AV ( $\leq 0.13$  mg KOH/g) without any pollutants from catalysts. The solid catalyst can be recovered easily by external magnetic field for recycles and is less corrosive to reactors than liquid acid (e.g.,  $\text{H}_2\text{SO}_4$ ). However, biodiesel with 90–92% purity of FAMES may have to be re-transesterified or blended with less portion to fossil diesel to achieve the international standards for biodiesel [44]. Another disadvantage of this process is that reaction conditions are under severe conditions (e.g., 220 °C and 6.5 MPa) as compared to the method with solid base catalysts (e.g., 94.9% biodiesel yield at 65 °C with  $\text{Na}_2\text{SiO}_3$  [27]). Therefore, further study is required to improve the catalyst activity for transesterification by loading strong base sites to become a bifunctional catalyst with both acidic and basic properties.

On the other hands, with the strong acidity, the catalyst can find applications in the esterification of FFAs from crude oils for pre-treatment at low temperatures (e.g., <100 °C [23]) and the hydrolysis of lignocelluloses under mild conditions (e.g., 140 °C [24]).

#### 4. Conclusions

A novel route with five steps by hydrothermal, pyrolysis and sulfonation processes was developed to synthesize a novel carbonaceous acid with high acid density and strong magnetism. For the magnetic core (Fe/C) synthesized by hydrothermal precipitation and pyrolysis, it is necessary to re-coat a carbonaceous layer to protect  $\text{Fe}_3\text{O}_4/\text{Fe}$  from leaching during sulfonation. Before sulfonation, the magnetic carbon (AC@Fe/C) needs pyrolysis step to achieve a suitable structure to load  $-\text{SO}_3\text{H}$  group and avoid leaching  $\text{Fe}_3\text{O}_4/\text{Fe}$ . It was found that pyrolysis temperature at 600 °C led to excellent structure to produce catalyst (AC-600- $\text{SO}_3\text{H}/\text{Fe}/\text{C}$ ) with high acid density (2.79 mmol/g) and strong magnetism (14.4  $\text{Am}^2/\text{kg}$ ). The catalyst presents high active, stable and recoverable in the production of *Jatropha* biodiesel with high yields for 3 cycles (90.5%, 91.8%, 90.3%), slight reduction in total acid density (2.43 vs. 2.79 mmol/g) and high catalyst recovery rate of 96.3%.

#### Acknowledgements

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#### Appendix A. Supplementary material

Supplementary data associated with this article can be found, in the online version, at <http://dx.doi.org/10.1016/j.apenergy.2015.06.044>.

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